



Rice Husk Waste as an Exothermic Material for a Riser Sleeve for Steel Casting

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Abstract. This research examines the suitability of rice husk waste as an exothermic material for a riser sleeve for use in steel casting production. Exothermic sleeves are used in the steel casting process to compensate for shrinkage of the steel during solidification. Commonly, the exothermic sleeve consists of fuel materials, fillers, and binders. Rice husk waste has potential for use as a fuel material in the exothermic sleeve due to its high calorific value. For this study, rice husk waste was ground to gain a particle size of 60 mesh and then mixed with organic binders of 12wt%, 15wt%, and 18wt%. A H-sleeve was then formed by hand pressing, followed by drying. A series of quantitative tests were carried out to analyze the performance of the rice husk as an exothermic material. These include measurement of modulus extension factor (MEF) and the cooling rate of the steel casting within the liquidus-solidus temperature range. The test results show that the rice husk sleeve mixed with 12wt% of binder extended the solidification time from 273 seconds to up to 511 seconds within the desired temperature range. Furthermore, the best MEF of 1.69 was achieved using the rice husk riser sleeve. This meets the standard MEF value of an exothermic sleeve.

Keywords: Exothermic sleeve; Modulus extension factor; Rice husk; Riser sleeve; Steel casting

1. Introduction

Exothermic riser sleeves are feeding aids used in steel casting to prevent the molten steel from shrinking during solidification. They perform better than silica sand risers (conventional risers) in increasing feeding efficiency and minimizing the riser size (Brown, 2000; Miki, 2002). One riser sleeve manufacturer reports that the use of an exothermic riser sleeve can enhance the casting yield by 74.47–91.80% (Schäfer, 2011). According to many references (Auderheide et al., 1999; Miki, 2002; Schäfer, 2011), exothermic riser sleeves consist of fuels (i.e., oxidizable metals or exothermic materials), fillers (i.e., sand or metal oxides), and binders (i.e., resin or water glass). In order for an exothermic riser sleeve to produce a high casting yield, certain parameters must be considered, such as the heat resistance of the fuel material in the exothermic sleeve, which should readily ignite at 600°C (Williams et al., 2015; Dafiqurrohman et al., 2016); the density of the exothermic sleeve, which should be low as porosity produces higher insulation (Miki, 2002); and the ash content after the material is burned (Rao, 2013). These properties are required to keep the retardation of temperature fall during steel

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solidification. In our previous studies (Idamayanti et al., 2015; Purwadi et al., 2016), we investigated an exothermic riser sleeve manufactured from aluminium slag and red mud waste. The results of these studies confirmed that the synergy of these materials resulted in excellent characteristics due to their exothermic and insulating behavior.

However, our previous studies revealed several problems, including limited raw materials and a complicated sleeve fabrication process. To solve these problems, substitute materials were studied based on their thermal properties. One study reported on an experiment in which rice husk was used as the primary material to produce a top riser sleeve to prevent heat loss from the mold (Rao, 2013). This showed the potential of rice husk for use in a riser sleeve. Currently, rice husk is not widely used in the foundry industry, despite its abundance as biomass waste in Indonesia (Gibran et al., 2018). It is a source of renewable energy and, due to its high calorific value (Lim et al., 2012), is promising as an exothermic material. Thus, this study aimed to utilize rice husk waste as a material for an exothermic riser sleeve. Rice husk has a remarkably higher heating value (15.84 MJ/kg) (Lim et al., 2012) than commercial exothermic sleeves (250–850 kJ/kg) (Williams et al., 2015). Burned rice husk produces combustion residues that contain SiO₂ (91.42%), K₂O (3.71%), CaO (3.21%), Al₂O₃ (0.78%), and small amounts of other metal oxides (Maiti et al., 2006), all of which can act as insulators. As well as being affordable and having slow oxidation properties, rice husk is one of the carbonaceous materials with anti-piping characteristics (Rao, 2013). Based on previous studies, it can be concluded that rice husk is a potential material for exothermic sleeves with its excellent physical properties (Maiti et al., 2006), effective insulating potential due to the amorphous structure of residual silica, and the high porosity of its ash residues (Wang et al., 2016a); (Tiwari and Pradhan, 2017). It is easy to form into briquettes with a low binder of 2–4% (Maiti et al., 2006) and is an eco-friendly product with very low emissions (Unrean et al., 2018).

Hence, this research focuses on the use of rice husk waste as an exothermic material for a riser sleeve in steel casting. Its suitability as a riser sleeve was determined quantitatively by testing the modulus extension factor (MEF) and measuring the cooling rate to observe the thermal behavior of the rice husk sleeve. Furthermore, the simulation was calculated to predict its feeding efficiency in steel casting. The physical properties of the rice husk sleeve, such as its bulk density and compressive strength, were also investigated.

2. Methods

2.1. Materials

The rice husk sleeve was formed by mixing rice husk waste, collected from a local rice mill, with acetate polymer, which is an organic binder made of technical grade material. To identify the performance of the rice husk sleeve in the feeding system, GX60Cr15, a high alloy steel, was selected. An elemental analysis of the GX60Cr15 alloy was conducted using an optical emission spectrometer (OES, research grade ARL 4360). The results are shown in Table 1.

The rice husk particles were prepared by milling and sieving to reduce and homogenize the size of the rice husk feedstock to within a range of 40 to 60 mesh. The higher heat value (HHV) of rice husk waste and a commercial sleeve (KALMINEX 2000) were measured using a bomb calorimeter and are shown in Table 2.

Table 1 Elemental analysis of GX60Cr15

Elements	%
C	0.638
Cr	14.925
Mn	0.618
Si	1.018
Mo	0.125
Ni	2.588
V	0.060
P	0.025
Fe	balance

Table 2 Higher heat value (HHV) of materials

Materials	HHV (MJ/kg)
Rice husk	15.3
KALMINEX 2000	11.3

2.2. Fabrication of Rice Husk Sleeve

The rice husk was mixed homogeneously with various amount of organic binder: 12%wt, 15%wt, and 18%wt. The mixture was molded and compacted by manual (hand) pressing to form a cylinder sleeve (H-sleeve type), as shown in Figure 1.

**Figure 1** Rice husk sleeve

The sleeve dimensions used for the observation were 80 mm in diameter, 15 mm in thickness, and 80 mm in height, with the modulus of the sleeve set accordingly to 1.38 cm. The last step was to dry the sleeve at 110°C for 1 hour.

2.3. Rice Husk Sleeve Characterizations

Characterizations were performed to identify the quality of the sleeve. Several characteristics of the rice husk sleeve were determined by referring to the standard specifications of IS 15865:2009 (The Foundry and Steel Castings Sectional Committee, 2009).

2.3.1. Compressive strength

The compressive strength of a sleeve should be 5.0 kg/cm² or higher. The whole sleeve was tested in compression mode until it fractured. The compressive strength was obtained by dividing the highest load of the sleeve by its average cross-sectional area. The compressive strength not only indicates the sleeve's resistance against the compressive

load, but also other properties associated with this load type, such as formability and stability during storage. The compressive strength was also used to determine the minimum binder content.

2.3.2. Bulk density

The bulk density of the sleeve was obtained by dividing the weight of the sleeve by its volume. The bulk density of the rice husk sleeve was in the range of 0.3–0.4 g/cm³. The degree of porosity, which is related to the bulk density of the sleeve, increases its insulation.

2.3.3. Cooling rate measurement

A thermocouple was installed in the center of the sleeve and attached to a data logger, which recorded the cooling temperature for 30 minutes. The experimental layout is illustrated in Figure 2. The data recording was carried out during the liquid state of the material ranging, from the pouring temperature to the liquidus temperature of GX60Cr15 (1340°C), which was then established as a working temperature range of the sleeve.

The solidification temperature of GX60Cr15 casting was measured for both the rice husk sleeve and the sand riser, while the KALMINEX sleeve was used as a reference sleeve.

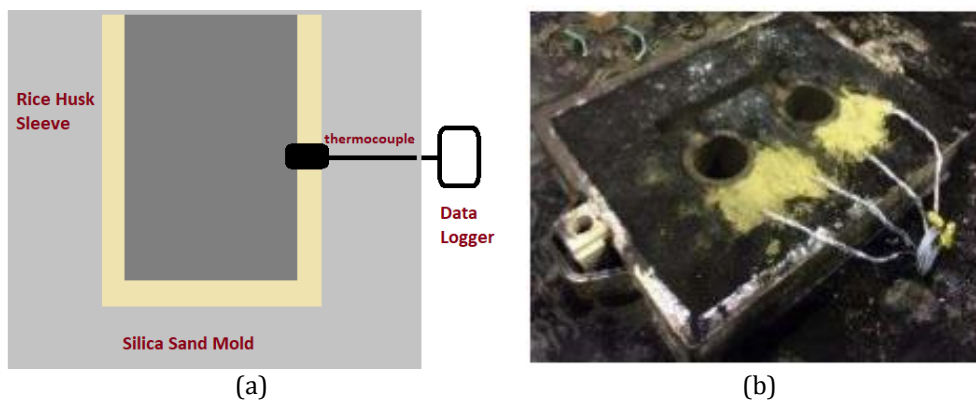


Figure 2 The layout for temperature measurement: (a) cross-section view; (b) top view

2.3.4. Modulus extension factor (MEF)

The ratio of a sand riser modulus to the sleeve modulus at the same retardation time is expressed as the MEF. The recommended MEF values by size are shown in Table 3 (The Foundry and Steel Castings Sectional Committee, 2009).

Table 3 The MEF criteria of a sleeve

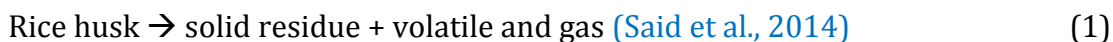
	Minimum MEF	
	Exothermic and insulating sleeves	Insulating sleeve
Up to 150 mm diameter	1.60	1.45
160 to 225 mm diameter	1.45	1.30
250 to 300 mm diameter	1.40	1.30
325 to 400 mm diameter	1.30	1.20
425 to 500 mm diameter	1.30	1.20
525 mm and above	1.30	1.20

3. Results and Discussion

3.1. Rice Husk as the Main Material of the Sleeve

Table 2 shows that the rice husk released heat energy to up to 15.3 MJ/kg. When the rice husk was applied as a riser sleeve, it resembled a pyrolysis reaction which burned at

250–600°C (Wang et al., 2016a). The reaction continued while the molten steel (approximately 1500°C) was poured, which led to the release of a considerable amount of heat and a subsequent extension of the solidification time. The first stage of the exothermic reaction in common biomass is hemicellulose decomposition, which released 40–280 kJ/kg of energy (Bates et al., 2013). The pyrolysis of rice husk, represented by the reaction scheme in Equation 1, is a thermochemical decomposition in which biomass organics are heated at high temperatures in the absence of oxygen and, therefore, decompose into solid carbon and volatile matter (Wang et al., 2016b; Quispe et al., 2017).



The temperature of the pyrolysis process influences the pyrolysis product. At 1200°C or higher, the mass fraction of pyrolysis gas (volatile matter) is higher than that of rice husk char and tar (Wang et al., 2016b). Xinyu Wang et al. concluded that pyrolysis gas is mostly released within 6 minutes (Wang et al., 2016b). The higher the temperature, the more gas is produced. Furthermore, CH₄ and CO gases are predominantly formed when rice husk sleeve is in direct contact with molten steel at 1500°C.

Furthermore, a previous study reported the measurement of the heat released during rice husk degradation (pyrolysis) using differential scanning calorimetry (Said et al., 2014). The results showed that there are several steps or zones in the pyrolysis of rice husk, namely the decomposition zone, the drying zone, the devolatilizing zone, and the char degradation zone. In the drying zone, the amount of heat absorbed by moisture is 161.5 kJ/kg, which is known as the endothermic process. In the devolatilizing zone, the released energy is 4437 kJ/kg, and in the char degradation zone, the energy absorbed is 313 kJ/kg (Said et al., 2014). The total energy involved in the pyrolysis of rice husk is determined as enthalpy decomposition energy (which is confirmed as the heating value). The mechanism of thermal degradation of rice husk has been thoroughly investigated and proves that rice husk has significant potential for use as the primary material in exothermic sleeves with a heat value that is higher than that of commercial sleeves.

3.2. Characterization of the Rice Husk Sleeve

3.2.1. Compression strength

Based on IS 15865:2009, the compression strength should be 5.0 kg/cm² or higher and, for that purpose, is controlled by adjusting the binder content. This study uses acetate polymer binder to bind the rice husk particles in various mass fractions of 12wt%, 15wt%, and 18wt%. As Figure 3 shows, the rice husk sleeve had a compression strength of 6.67 kg/cm², 11.02 kg/cm², and 16.26 kg/cm², respectively. Subsequently, the rice husk sleeve was formed using a binder content of 12wt%, 15wt%, and 18wt%. The higher the binder content, the better the formability of the sleeve.

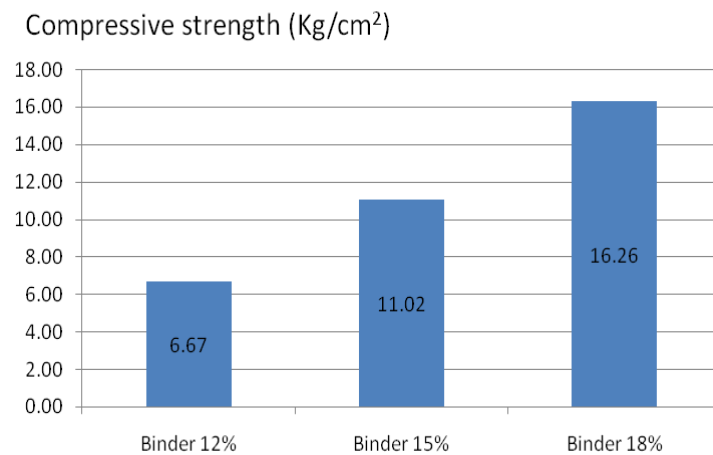


Figure 3 The compressive strength of the rice husk sleeve

3.3. Thermal Behavior of the Rice Husk Sleeve

The effectiveness of an exothermic sleeve is determined by the duration necessary for the sleeve to retard the solidification of the steel in the riser. Furthermore, heat released by the exothermic reaction can delay the formation of a solid shell in the early stages of steel solidification (Midea et al., 2007). The burning of the sleeve involves several stages take: ignition, combustion, time to reach maximum temperature, and insulation.

The temperature of the GX60Cr15 casting was measured over 30 minutes. As shown in Figure 4, the ideal temperature range of rice husk sleeve was determined as 1340°C (liquidus temperature) or above.

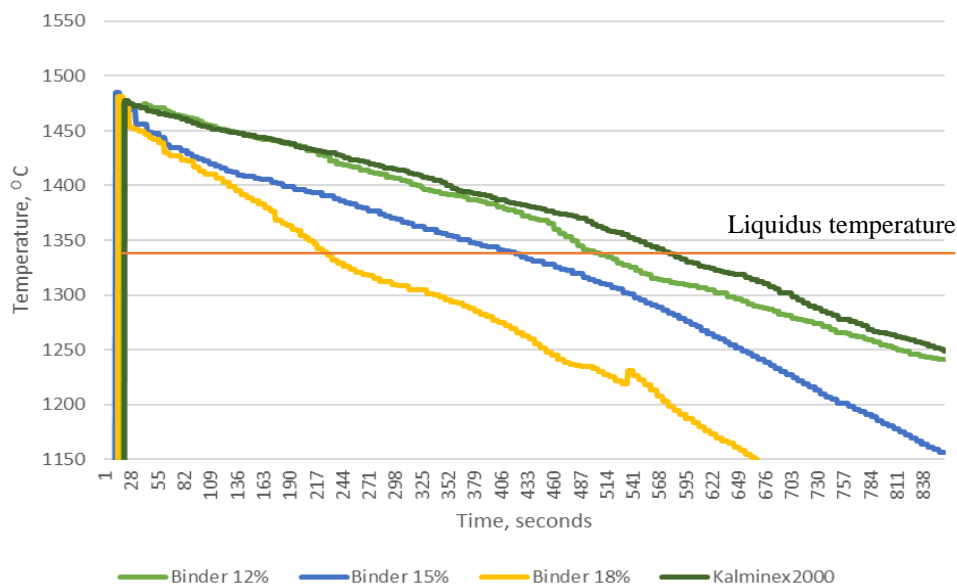


Figure 4 Cooling rate of GX60Cr15 solidification using the rice husk sleeve expressed as a function of binder content

The rice husk sleeve performed best with a binder content of 12%wt as it maintained the temperature of molten metal above 1340°C for up to 511 seconds. The binder content of 15%wt and 18%wt kept the molten steel above liquidus temperature for 409 seconds and 237 seconds, respectively. These results indicate that the binder content has a significant influence on temperature retardation as shown it determines the amount of rice

husk ash that forms after the burning process, which contributes to the insulating effect. The lower the binder content of a sleeve, the more rice husk ash formed. The characteristics of rice husk ash include good refractoriness (which depends primarily on its alkali oxides content), high porosity, light weight and bulkiness (Kapur, 1980). The porosity of the rice husk sleeve enhances its insulating capability (Kaviany, 1995) to prevent heat loss and prolong the solidification time, as illustrated in Figure 5. This is because the porosity of the sleeve is related to its compression strength. For example, a compression strength of 16 kg/cm² resulted from a porosity of 68% (Kapur, 1980).

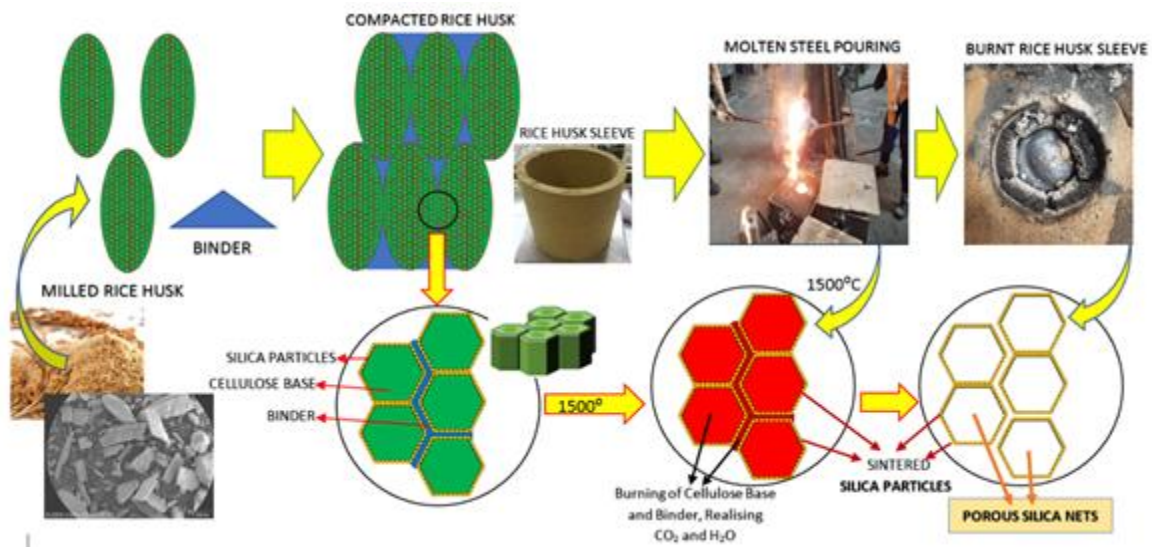


Figure 5 Illustration of porous silica net formation as a result of burning the rice husk sleeve

Table 4 The modulus of sand riser and sleeve in relation to retardation time

Sand riser Dimensions Diameter (∅) mm, Height (H) mm	Volume (mm ³) Heat releasing area (mm ²)	Modulus, cm	Retardation time, s	Modulus extension factor (MEF) = sand/sleeve
∅80 mm, H 80 mm	444 / 32.2	1.38	215	
∅90 mm, H 90 mm	625 / 40.5	1.54	278	
∅100 mm, H 100 mm	867 / 50.4	1.72	342	
∅110 mm 110 mm	1.164 / 61.3	1.90	409	
∅130 mm 120 mm	1.592 / 755	2.1	436	
∅140 mm, 140 mm	2.155 / 923	2.33	454	
∅140 mm, 150 mm	2.474 / 1.013	2.44	527	
Rice husk sleeve binder 12%wt	443.677 / 32.2	1.38	511	2.33/1.38 = 1.69
Rice husk sleeve binder 15%wt	443.677 / 32.2	1.38	409	1.90 / 1.38 = 1.46
Rice husk sleeve binder 18%wt	443.677 / 32.2	1.38	237	1.54 / 1.38 = 1.12
KALMINEX 2000	443.677 / 32.2	1.38	579	2.44 / 1.38 = 1.77

The performance of an exothermic sleeve is also quantified by measuring the MEF, which represents the increase in the modulus of the riser (Rao, 2013). The higher the MEF value, the smaller the dimensions of the sleeve. The MEF calculation is presented in Table 4, where the standard modulus of a sand riser is determined as 1.38. As Figure 6 demonstrates, the binder content influenced the MEF results. A binder content of 12wt %,

15wt%, and 18wt% produced MEF values of 1.12, 1.38, and 1.69, respectively. With a binder content of 12wt%, the rice husk sleeve has an MEF value close to that of a commercial sleeve (KALMINEX 2000) and can, therefore, be classified as an exothermic sleeve.

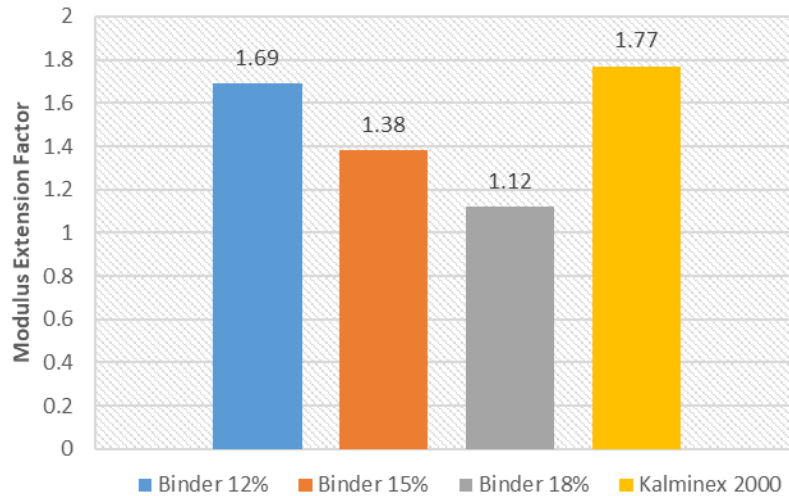


Figure 6 Modulus extension factor of the sleeves

The feeding efficiency of the rice husk sleeve can be simulated by taking a binder content of 12wt% and an MEF value of 1.69 and following the calculation steps in Equations 2 to 4 below (The Foundry and Steel Castings Sectional Committee, 2009).

$$\text{Modulus of the sleeve } (M_s) = (D \times H) / (D+4H) \quad (2)$$

$$\text{Equivalent modulus of the sand riser } (M_{sr}) = \text{MEF}_{\text{sleeve}} \times M_s \quad (3)$$

$$\text{Feeding efficiency of rice husk sleeve} = (V_{sr} / V_s) \times 100\% \quad (4)$$

First, the modulus of the sleeve (M_s) is calculated using Equation 2, where D (diameter) is 8 cm, and H (height) is 8 cm. The M_s obtained is 1.6 cm and the M_{sr} is 2.704 cm. The real volume of the sand riser (V_{sr}) is 1940 cm³ and the volume of the sleeve (V_s) is 401.92 cm³. Assuming that the sand riser efficiency is 14%, the molten steel supplies 271.60 cm³. Thus, the feeding efficiency of the rice husk sleeve based on the previous equations is 67.58%. Therefore, by using the rice husk sleeve as a riser, the feeding efficiency can be increased to 67.58%.

4. Conclusions

Rice husk waste has significant potential for use as a material for a riser sleeve feeding system in steel casting. The MEF calculation generates an MEF value of 1.69, based on which the rice husk sleeve can be classified as an exothermic sleeve. With a binder content of 12wt%, the rice husk sleeve had good formability, a sufficient compressive strength of 6.9 kg/cm², and excellent temperature retardation of during GX60Cr15 solidification. The solidification time of molten metal in the rice husk sleeve can be extended to 511 seconds, which is higher than that of the sand riser (215 seconds). Furthermore, the feeding efficiency of the rice husk sleeve can be increased to approximately 67.58%. In terms of compliance, the main characteristics of the rice husk sleeve comply with the standard specifications of IS 15865:2009 for an exothermic sleeve. Hence, the rice husk sleeve is

recommended for use in a feeding system for steel casting, where it has the potential to replace existing commercial exothermic sleeves and enhance the value of rice husk waste.

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